A multilayer Saint-Venant system with mass exchange

September 22, 2009

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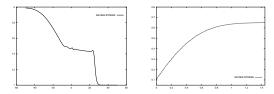
Existing models for free surface flows

Incompressible Navier Stokes equations

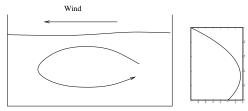
- Efficient model for a large class of flows
- Complex implementation (moving boundaries)
- CPU time (3d computations)
- Robustness of the softwares for stiff flows (dam break,...)
- Shallow water equations
 - Easy implementation (fixed domain)
 - CPU time (2d computations)
 - Robustness of the software
 - Agreement with experiments... but not for all flows !
 - Constant velocity along the z-direction
 - Hydrostatic approximation

Two flows for which SW model fails

Strong friction on the bottom \rightsquigarrow Vertical dependency for u



▶ Wind stress in a lake ~→ Wind-induced circulation process



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A multilayer SW model : The bi-fluid SW model

Introduced by Castro M., Macias J. and Pares C. (2001)

$$(BF) \begin{cases} \frac{\partial h_1}{\partial t} + \nabla \cdot (h_1 u_1) = 0, \\\\ \frac{\partial h_1 u_1}{\partial t} + \nabla \cdot (h_1 u_1 \otimes u_1) + \nabla (\frac{g}{2} h_1^2) = -\frac{\rho_2}{\rho_1} g h_1 \nabla h_2 \\\\\\ \frac{\partial h_2}{\partial t} + \nabla \cdot (h_2 u_2) = 0, \\\\\\ \frac{\partial h_2 u_2}{\partial t} + \nabla \cdot (h_2 u_2 \otimes u_2) + \nabla (\frac{g}{2} h_2^2) = -g h_2 \nabla h_1 \end{cases}$$

→ Pares et al. ('04,'07), Kurganov ('08), Abgrall-Karni ('08), Bouchut et al. ('08, '09)

From NS equations to multilayer SW models

Derivation (following Gerbeau-Perthame...)

- ► Formal asymptotic analysis of NS equ. under SW assumption
- Vertical discretization of the fluid into N layers
- Vertical integration of approximated NS equations by layer
- Consequences
 - Each layer has its own velocity
 - Coupling between the layers through
 - Pressure term (global coupling)
 - Mass exchange (local (?) coupling : interface condition for mass equation)
 - Viscous effect

(local coupling : interface condition for momentum equation)

Hydrostatic incompressible Euler equ. with free surface

$$\begin{cases} \frac{\partial u}{\partial x} + \frac{\partial w}{\partial z} = 0, \\\\ \frac{\partial u}{\partial t} + \frac{\partial u^2}{\partial x} + \frac{\partial uw}{\partial z} + \frac{\partial p}{\partial x} = 0, \\\\ \frac{\partial p}{\partial z} = -g, \end{cases}$$

with

$$t > 0, \quad x \in \mathbb{R}, \quad z_b(x) \le z \le \eta(t, x),$$

and two kinematic boundary conditions (free surface and bottom)

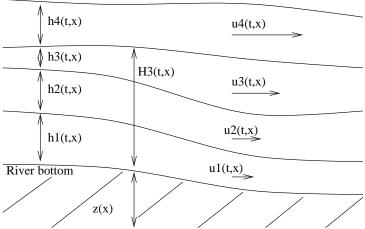
$$\frac{\partial \eta}{\partial t} + u_s \frac{\partial \eta}{\partial x} - w_s = 0$$

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Multilayer approach





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Vertical integration on a layer

$$\begin{aligned} \frac{\partial}{\partial t}h_{\alpha} + \frac{\partial}{\partial x}h_{\alpha}\bar{u}_{\alpha} &= \mathbf{G}_{\alpha+1/2} - \mathbf{G}_{\alpha-1/2}, \\ \frac{\partial}{\partial t}h_{\alpha}\bar{u}_{\alpha} + \frac{\partial}{\partial x}h_{\alpha}\bar{u}_{\alpha}^{2} + \mathbf{g}h_{\alpha}\frac{\partial}{\partial x}H \\ &= -\mathbf{g}h_{\alpha}\frac{\partial}{\partial x}z_{b} + \mathbf{u}_{\alpha+1/2}\mathbf{G}_{\alpha+1/2} - \mathbf{u}_{\alpha-1/2}\mathbf{G}_{\alpha-1/2} \end{aligned}$$

with the mass exchange term

$$G_{\alpha+1/2} = \frac{\partial}{\partial t} z_{\alpha+1/2} + u_{\alpha+1/2} \frac{\partial}{\partial x} z_{\alpha+1/2} - w_{\alpha+1/2}$$

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Vertical integration on a layer

$$\begin{aligned} \frac{\partial}{\partial t}h_{\alpha} + \frac{\partial}{\partial x}h_{\alpha}\bar{u}_{\alpha} &= \mathbf{G}_{\alpha+1/2} - \mathbf{G}_{\alpha-1/2}, \\ \frac{\partial}{\partial t}h_{\alpha}\bar{u}_{\alpha} + \frac{\partial}{\partial x}h_{\alpha}\bar{u}_{\alpha}^{2} + gh_{\alpha}\frac{\partial}{\partial x}H \\ &= -gh_{\alpha}\frac{\partial}{\partial x}z_{b} + u_{\alpha+1/2}\mathbf{G}_{\alpha+1/2} - u_{\alpha-1/2}\mathbf{G}_{\alpha-1/2} \end{aligned}$$

with the mass exchange term

$$\mathcal{G}_{lpha+1/2} = \sum_{1}^{lpha} rac{\partial}{\partial t} h_eta + rac{\partial}{\partial x} h_eta ar{u}_eta$$

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Vertical integration on a layer

$$\begin{aligned} \frac{\partial}{\partial t}h_{\alpha} &+ \frac{\partial}{\partial x}h_{\alpha}\bar{u}_{\alpha} = G_{\alpha+1/2} - G_{\alpha-1/2}, \\ \frac{\partial}{\partial t}h_{\alpha}\bar{u}_{\alpha} &+ \frac{\partial}{\partial x}h_{\alpha}\bar{u}_{\alpha}^{2} + gh_{\alpha}\frac{\partial}{\partial x}H \\ &= -gh_{\alpha}\frac{\partial}{\partial x}z_{b} + u_{\alpha+1/2}G_{\alpha+1/2} - u_{\alpha-1/2}G_{\alpha-1/2} \end{aligned}$$

Natural conditions for lowest and uppest layers

$$G_{1/2} = G_{N+1/2} = 0$$

Which choice for the others ?

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Multilayer system without mass exchange

$$G_{\alpha+1/2} = 0 \qquad \forall \ \alpha = 0, ..., N$$

- Energy inequality (global stability)
- Loss of hyperbolicity (interface stability)
- Non conservativity
- Kinetic interpretation (kinetic scheme)
- Numerical agreement with NS solutions for several test cases
- ▶ No physical meaning for the condition on $G_{\alpha+1/2}$
- Not adapted for wind-induced circulation processes

Wind-induced circulation process

Mass equation for each layer

$$\frac{\partial}{\partial t}h_{\alpha} + \frac{\partial}{\partial x}h_{\alpha}\bar{u}_{\alpha} = \mathbf{0}$$

Boundary conditions

$$\bar{u}_{lpha} = 0$$
 (Walls)

Stationnary solution

$$\bar{u}_{\alpha} = 0$$

 \rightsquigarrow Unrealistic !

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Multilayer SV model with mass exchange

- No a priori prescription for $G_{\alpha+1/2}$
- Mass equation for one layer is not meaningfull

$$\frac{\partial}{\partial t}h_{\alpha} + \frac{\partial}{\partial x}h_{\alpha}\bar{u}_{\alpha} = \mathbf{G}_{\alpha+1/2} - \mathbf{G}_{\alpha-1/2}$$

with $G_{\alpha+1/2} = \partial_t z_{\alpha+1/2} + u_{\alpha+1/2} \partial_x z_{\alpha+1/2} - w_{\alpha+1/2}$

We consider a single mass equation for the whole flow

$$rac{\partial}{\partial t}H+rac{\partial}{\partial x}\sum_{1}^{N}h_{lpha}ar{u}_{lpha}=0, \qquad h_{lpha}(t,x)=\lambda_{lpha}H(t,x), \qquad \sum_{1}^{N}\lambda_{lpha}=1$$

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Multilayer SV model with mass exchange

Momentum equation is now well defined

$$\lambda_{\alpha} \frac{\partial}{\partial t} H \bar{u}_{\alpha} + \lambda_{\alpha} \frac{\partial}{\partial x} H \bar{u}_{\alpha}^{2} + g \lambda_{\alpha} \frac{\partial}{\partial x} H^{2}$$
$$= -g \lambda_{\alpha} H \frac{\partial}{\partial x} z_{b} + u_{\alpha+1/2} G_{\alpha+1/2} - u_{\alpha-1/2} G_{\alpha-1/2}$$

with

$$G_{\alpha+1/2} = \sum_{1}^{\alpha} \left(\frac{\partial}{\partial x} h_{\beta} \bar{u}_{\beta} - \lambda_{\beta} \sum_{1}^{N} \frac{\partial}{\partial x} h_{\gamma} \bar{u}_{\gamma} \right)$$

Open question : Choice of $u_{\alpha+1/2}$

$$u_{\alpha+1/2} = \begin{cases} u_{\alpha} & \text{if} \quad G_{\alpha+1/2} \leq 0\\ u_{\alpha+1} & \text{if} \quad G_{\alpha+1/2} > 0 \end{cases}$$

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Properties of the new multilayer system

- System of N + 1 equations (including non conservative products)
- Entropy inequality for the total energy

$$E^{mc}(x,t) = \sum_{lpha=1}^{N} rac{h_lpha u_lpha^2}{2} + rac{gh_lpha (\eta+z_b)}{2}$$

 \rightsquigarrow ensures a global stability for the flow

- Hyperbolicity
 - ► Study includes the momentum exchange terms $u_{\alpha+1/2}G_{\alpha+1/2}$
 - True for the two layers system (whatever the choice of $u_{3/2}$)
 - Sometimes wrong if there is more than four layers

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Kinetic interpretation

Classical Saint-Venant system : (h, hu) is a solution if

$$M(t,x,\xi) = rac{h(t,x)}{c} \ \chi(rac{\xi - \mathbf{u}(t,x)}{c}), \qquad c = \sqrt{gh/2}$$

is solution of

$$\frac{\partial M_{\alpha}}{\partial t} + \xi \frac{\partial M_{\alpha}}{\partial x} = Q(t, x, \xi)$$

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Kinetic interpretation

Multilayer Saint-Venant system : (H, u^{mc}) is a solution if

$$M_{\alpha}(x,t,\xi) = l_{\alpha} rac{H(x,t)}{c} \chi\left(rac{\xi - u_{lpha}(x,t)}{c}
ight), \qquad c = \sqrt{gh/2}$$

are solutions of

$$\frac{\partial M_{\alpha}}{\partial t} + \xi \frac{\partial M_{\alpha}}{\partial x} - \frac{-N_{\alpha+1/2}(x,t,\xi) + N_{\alpha-1/2}(x,t,\xi)}{-N_{\alpha+1/2}(x,t,\xi)} = Q_{\alpha}(x,t,\xi)$$

where

$$N_{\alpha+1/2}(x,t,\xi) = G_{\alpha+1/2}(x,t) \,\delta\left(\xi - u_{\alpha+1/2}(x,t)\right),$$

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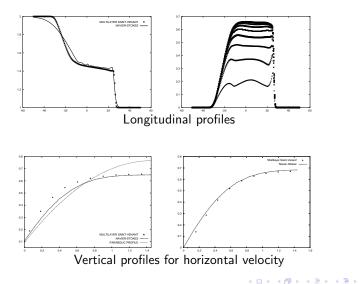
Numerical scheme

- Hyperbolic part : Kinetic scheme
 - Integration of upwind scheme for linear kinetic equations
 - ► No need for computation of the eigenvalues of the system
 - Stability under a modified CFL condition

$$\Delta t^{n} \leq \frac{l_{\alpha}H_{i}^{n}\Delta x_{i}}{l_{\alpha}H_{i}^{n}\left(|u_{\alpha,i}^{n}|+w_{M}c_{i}^{n}\right)+\Delta x_{i}\left(\left[G_{\alpha+1/2,i}^{n+1/2}\right]_{-}+\left[G_{\alpha-1/2,i}^{n+1/2}\right]_{+}\right)}$$

- Topographic terms : Hydrostatic reconstruction
- ► Viscous terms : Implicit computation of momentums → Solution of a well-posed tridiagonal N × N system

1d Dam Break



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Wind-induced circulation : hydrostatic NS solutions

Stationnary solution far from the boundaries $(u_{\alpha} = cst)$

$$\partial_x \mathbf{p} = \nu \partial_{zz} \mathbf{u}$$

Hydrostatic assumption and boundary conditions

 $\nu \partial_z u = \tau$ (Surface), $\nu \partial_z u = \kappa u$ (Bottom)

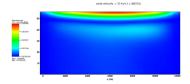
Solution for large κ

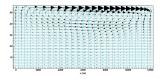
$$\partial_x h = \frac{3\tau}{2gh}, \qquad u(\xi) = 2\xi(\frac{3\xi}{2} - 1), \quad \xi = \frac{z}{h} \in [0, 1]$$

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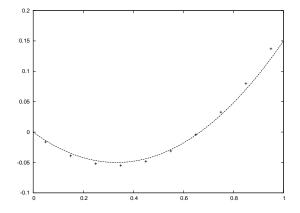
Wind-induced circulation : Multilayer solution





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Wind-induced circulation : Multilayer solution



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Multilayer SW vs. NS equations : CPU Time

CPU time

 2D Navier-Stokes equations : MISTRAL software by J.F. Gerbeau and T.Lelievre (ALE, implicit solver...)

 \rightarrow CPU Time = 23.77 seconds (35 time steps)

ID Saint-Venant system

 \rightarrow CPU Time = 0.07 second (73 time steps)

Multilayer Saint-Venant system

 \rightarrow CPU Time = 1.19 second (76 time steps)

- Friction $\kappa = 0.1$
- Viscosity $\mu = 0.01$
- Ten layers (Navier-Stokes and multilayer SV system)