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## Erratum

# Numerical modelling of foam Couette flows

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We have found a technical error in Appendix A of [1] which induced errors in Appendix B and in the figures. However, the text of the paper, including all conclusions drawn, is completely unaffected by the changes. In [1], equations (A.1a), (A.1b), and (A.1c) should read

$$\lambda \frac{\partial \tau_{rr}}{\partial t} + \max \left( 0, 1 - \frac{\tau_Y}{|\boldsymbol{\tau}_d|} \right) \tau_{rr} = 0, \quad (\text{A.1a})$$

$$\lambda \left( \frac{\partial \tau_{r\theta}}{\partial t} - 2\dot{\epsilon}_{r\theta} \tau_{rr} \right) + \max \left( 0, 1 - \frac{\tau_Y}{|\boldsymbol{\tau}_d|} \right) \tau_{r\theta} = 2\eta \dot{\epsilon}_{r\theta}, \quad (\text{A.1b})$$

$$\lambda \left( \frac{\partial \tau_{\theta\theta}}{\partial t} - 4\dot{\epsilon}_{r\theta} \tau_{r\theta} \right) + \max \left( 0, 1 - \frac{\tau_Y}{|\boldsymbol{\tau}_d|} \right) \tau_{\theta\theta} = 0, \quad (\text{A.1c})$$

with  $\dot{\epsilon}_{r\theta} = 1/2 \left( \frac{\partial v}{\partial r} - \frac{v}{r} \right)$ . Consequently, Appendix B is modified but its conclusion remains the same: if the strain rate is discontinuous, we can predict the critical strain rate

$$\dot{\epsilon}_{r\theta}^c = \frac{1}{2\eta} \left[ 1 - \frac{\tau_Y}{\sqrt{2} |\tau_{r\theta}(r_c)|} \frac{1}{\left( 1 + \frac{\lambda^2}{\eta^2} \tau_{r\theta}(r_c)^2 \right)^{1/2}} \right] \tau_{r\theta}(r_c).$$

All the presented computations have been made again,

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and most figures are unchanged, except Figures 7, 8(b), and 9(b), whose new versions are shown in the following page.

### Modified Appendix B

[...] We write the constitutive equation with  $\frac{\partial}{\partial t} = 0$ . We have:

– When  $r > r_c$ : the plasticity term is zero, so (A.1c) leads to  $2\lambda \dot{\epsilon}_{r\theta} \tau_{r\theta} = 0$ , and  $\dot{\epsilon}_{r\theta} = 0$  as  $\tau_{r\theta} \neq 0$ ; in addition, we have  $v = 0$  because of boundary conditions. However, (A.1a) and (A.1b) are then equivalent to  $0 = 0$ , and the normal stress components are not determined by the stationary equations only. In the transient problem, their values are determined by the initial conditions. Finally, as  $v = 0$ , (A.2b) yields  $\tau_{r\theta} = C/r^2$ , where  $C$  is a constant.

– When  $r < r_c$ : (A.1a, A.1b) lead to

$$\begin{aligned} \left( 1 - \frac{\tau_Y}{|\boldsymbol{\tau}_d|} \right) \tau_{rr} &= 0, \\ -2\lambda \dot{\epsilon}_{r\theta} \tau_{rr} + \left( 1 - \frac{\tau_Y}{|\boldsymbol{\tau}_d|} \right) \tau_{r\theta} &= 2\eta \dot{\epsilon}_{r\theta}, \\ -4\lambda \dot{\epsilon}_{r\theta} \tau_{r\theta} + \left( 1 - \frac{\tau_Y}{|\boldsymbol{\tau}_d|} \right) \tau_{\theta\theta} &= 0. \end{aligned}$$

We denote with  $a^-$  (respectively,  $a^+$ ) the quantities evaluated in  $r = r_c^-$  (respectively in  $r = r_c^+$ );  $v$  and  $\tau_{r\theta}$  are continuous, thus  $v^- = v^+ = 0$ ,  $\tau_{r\theta}^- = \tau_{r\theta}^+ = \tau_{r\theta}(r_c)$  and we

have

$$\begin{aligned} \left(1 - \frac{\tau_Y}{|\tau_d^-|}\right) \tau_{rr}^- &= 0, \\ -2\lambda \dot{\epsilon}_{r\theta}^- \tau_{rr}^- + \left(1 - \frac{\tau_Y}{|\tau_d^-|}\right) \tau_{r\theta}(r_c) &= 2\eta \dot{\epsilon}_{r\theta}^-, \\ -4\lambda \dot{\epsilon}_{r\theta}^- \tau_{r\theta}(r_c) + \left(1 - \frac{\tau_Y}{|\tau_d^-|}\right) \tau_{\theta\theta}^- &= 0. \end{aligned}$$

If  $1 - \frac{\tau_Y}{|\tau_d^-|} = 0$ , we find  $\dot{\epsilon}_{r\theta}^- = 0 = \dot{\epsilon}_{r\theta}^+$ : there is no discontinuity.

If  $1 - \frac{\tau_Y}{|\tau_d^-|} \neq 0$ , we find

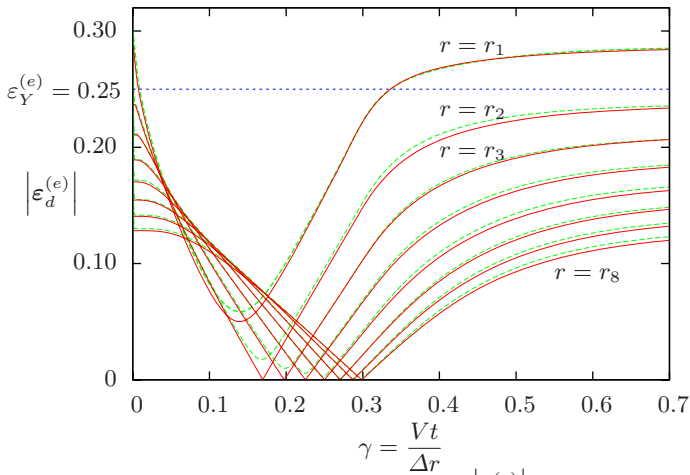
$$\begin{aligned} \tau_{rr}^- &= 0, \\ \tau_{\theta\theta}^- &= 2\frac{\lambda}{\eta} \tau_{r\theta}(r_c)^2, \\ \dot{\epsilon}_{r\theta}^- &= \frac{1}{2\eta} \left(1 - \frac{\tau_Y}{|\tau_d^-|}\right) \tau_{r\theta}(r_c), \end{aligned}$$

with now

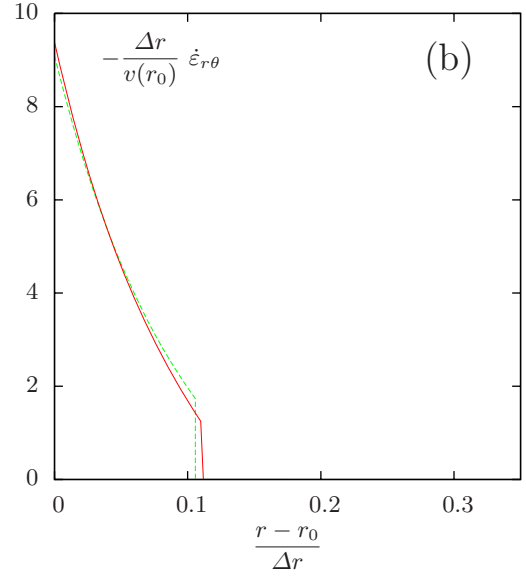
$$|\tau_d^-| = \left(2\tau_{r\theta}(r_c)^2 + 2\frac{\lambda^2}{\eta^2} \tau_{r\theta}(r_c)^4\right)^{1/2}.$$

As  $\dot{\epsilon}_{r\theta}^- \neq \dot{\epsilon}_{r\theta}^+$ , the strain rate is discontinuous at  $r = r_c$  and we can define a critical strain rate

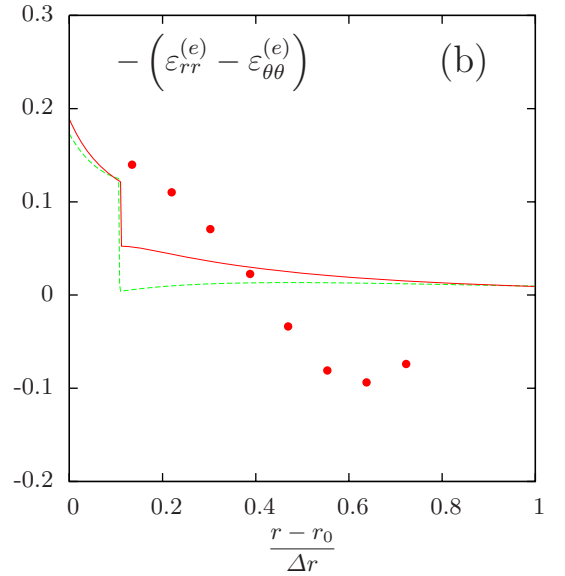
$$\dot{\epsilon}_{r\theta}^c = \frac{1}{2\eta} \left[1 - \frac{\tau_Y}{\sqrt{2}|\tau_{r\theta}(r_c)|} \frac{1}{\left(1 + \frac{\lambda^2}{\eta^2} \tau_{r\theta}(r_c)^2\right)^{1/2}}\right] \tau_{r\theta}(r_c).$$



**Fig. 7.** (Colour online) Transient case:  $|\epsilon_d^{(e)}|$  versus  $t$  for  $r$  from  $r = r_1$  to  $r_8$ . Dashed green lines: former computations; solid red lines: present computations.



**Fig. 8.** (Colour online) Stationary case: (b) Shear strain rate  $\dot{\epsilon}_{r\theta}$  versus  $r$ . There is no experimental data available for the comparison. Dashed green lines: former computations; solid red lines: present computations.



**Fig. 9.** (Colour online) Stationary case: (b) Difference of normal components.  $-\left(\epsilon_{rr}^{(e)} - \epsilon_{\theta\theta}^{(e)}\right)$  versus  $r$ . Dashed green lines: former computations; solid red lines: present computations;  $\bullet$ : experimental data.

## References

1. I. Cheddadi, P. Saramito, C. Raufaste, P. Marmottant, F. Graner, *Eur. Phys. J. E* **27**, 123 (2008).